MODELING THE CATALYTIC REDUCING OF N₂O AMOUNT IN NITRIC ACID PRODUCTION O.N. Bliznjuk, N.F. Kleshchev, A.N. Ogurtsov, National Technical University "Kharkiv Polytechnic Institute" onbliznjuk@ukr.net

Currently, the only industrial process for producing nitric acid is the catalytic oxidation of ammonia with oxygen from the air, followed by absorption of nitrogen oxides produced by water. The stage of NH₃ change ratio largely determines the performance of all nitric acid production. The conditions and the quality of its implementation determine the consumption indices of NH₃, input and losses of platinum group metals (PGM) and energetic capabilities of process conditions.

The studies conducted [1-5] justify the assumption about the mechanism of the ammonia catalytic oxidation on platinoid gauzes, give a kinetic model of the reaction, and allow us to determine the conditions of maximum NO output. As the analysis of the bibliography and our experimental research has shown, to ensure the maximum NO selectivity and high intensity of the process it is necessary to maintain external diffusion conditions. At low NH₃ concentrations of the catalyst surface, which is typical for external diffusion conditions, the rates of its oxidation to N₂O and N₂ decrease dramatically and NH₃ selective oxidation to NO takes place.

One of the shortcomings of previous studies and previously-developed models is the lack of data on the nitrogen oxide formation developed as a byproduct by NH_3 catalytic oxidation in the HNO_3 manufacture process. Nitrogen oxide passes through the remaining stages of the HNO_3 production technology unchanged and then is released into the atmosphere. The facilities for the nitric acid manufacture in the CIS countries currently emit about 6.0–7.5 kg of N₂O per year per ton of HNO_3 . According to the latest research N₂O is a strong greenhouse gas, whose global warming potential is 310 times greater than the one of CO_2 . To create a mathematical model of the ammonia oxidation to NO with due consideration of N₂- and N₂O-synthesis, a complex of physicochemical, kinetic and technological research has been carried out.

Taking to account the formation of nitrogen (I) oxide for a PGM-catalyst, the stoichiometric basis of ammonia oxidation reaction routes, has the following form:

$$4\mathrm{NH}_3 + 5\mathrm{O}_2 \xrightarrow{k_1} 4\mathrm{NO} + 6\mathrm{H}_2\mathrm{O},\tag{1}$$

$$4NH_3 + 4O_2 \xrightarrow{k_2} 2N_2O + 6H_2O \tag{2}$$

$$4NH_3 + 3O_2 \xrightarrow{k_3} 2N_2 + 6H_2O \tag{3}$$

$$2NO \xrightarrow{k_4} N_2 + O_2 \tag{4}$$

Modelling of the process is reduced to a mathematical description of the process in the catalyst bed considering the assumed reaction mechanism. At a high temperature oxygen on the platinum surface is mainly in the dissociated state. The ammonia adsorption, as well as its dissociation and formation of intermediates interacting with each other, leads to the formation of NO, N₂O, N₂, H₂O and desorption from the free catalyst surface at 973–1193 K. In the process of catalysis the ammonia acts as an electron-donor, and oxygen – as an electron-acceptor. Adsorbed O_2 molecules attach electrons from the catalyst surface and turn into oxygen surface atoms. NH₃ molecule donates electrons from the catalyst surface which is not covered with oxygen, N-H bonds are thus weakening and the imido-particles are being formed. On the catalyst surface coated with oxygen, the ammonia forms particles of the imide-type, which are then recombining and form the nitrogen. Further addition of oxygen to the imide leads to the formation of NO. Other steps are connected with N₂O, N₂ and H₂O formation.

The proposed detailed mechanism of the process has been used for deriving kinetic equations, which describe the reactions on the catalyst surface and relate to the formation of O, N_2O , N_2 .

The process in the catalyst bed for external diffusion condition is characterized by a large temperature gradient. At a small distance - a few centimeters in front of the catalyst – the gas is

heated by the amount of the adiabatic heating of the reaction mixture from 473 to 1173 K. This can lead to significant longitudinal heat and mass transfer. However, the effective coefficients of longitudinal diffusion and thermal conductivity of the gas phase are small and longitudinal heat transfer is carried out mainly along the solid skeleton of the catalyst bed. When describing the process the influence of the flows arising in non-isothermal boundary layer of multi-component mixture - Stefan flow, thermal diffusion, as well as diffusion thermal conductivity can be neglected, since the volume of the reaction mixture does not vary by more than 10%, and it is highly diluted with inert gas N₂; molecular weights of components and, thus, their diffusion coefficients differ insignificantly. The temperature of the catalyst in the bed of PGM-gauzes is assumed to be constant and is determined by the adiabatic heating of the coming reaction mixture. On this basis, to describe the process, a model of plug-flow for the gas phase is accepted with the use of material balance equations for each component.

The degree of NH₃ oxidation on PGM-catalysts was calculated according to the developed mathematical model. For calculating this process it is necessary to know the coefficients of heat and mass transfer from the gas flow to the catalyst, as well as the physical and chemical properties of the mixture, depending on the temperature, pressure and composition of the mixture.

By solving the inverse problem of chemical kinetics, using the experimental data, we determined reactions rates constants connected with the formation of NO (k_1), N₂O (k_2), N₂ (k_3) and N₂, resulting from the nitrogen (II) oxide decomposition (k_4), and the concentrations of the substances on the catalyst surface. The comparison of calculated and experimental conversion coefficients shows good agreement, the difference is not more than 1–3%.

A mathematical model of the oxidation process of NH_3 , considering the physical and chemical properties of the ammonia-air mixture and nitrous gas has been developed. The rate constants and their temperature dependence have been determined. This will allow to determine the optimal process conditions of NH_3 oxidation on the PGM-catalyst at different pressures in a wide range of process parameters, as well as to determine the amount of nitrogen oxides N_2O formed. On the basis of the developed model, a program for calculating the NH_3 oxidation reactor using PGMcatalysts of different geometric profile has been created. During the operation process, the volume and the surface of the catalyst are changed. Thus the mathematical model for the rates of ammonia oxidation steps per unit mass of PGM-catalyst has been developed.

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